# **Geomagnetic Dynamo Theory**

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#### Introduction

Basic electrodynamics Kinematic, turbulent dynamos Magnetohydrodynamical dynamos Geodynamo simulations Need of a geodynamo Homopolar dynamo Geodynamo hypothesis

## Need of a geodynamo

- Earth and many other celestial bodies possess a large-scale, often variable magnetic field
- Decay time  $\tau = L^2/\eta$ magnetic diffusivity  $\eta = c^2/4\pi\sigma$ , electrical conductivity  $\sigma$
- Earth  $\tau \approx 20\,000$  yr
- Variability of geomagnetic field
- Dynamo:  $u \! \times \! B \sim j \sim B \sim u$

Faraday Ampere Lorentz motion of an electrical conductor in an 'inducing' magnetic field  $\sim$  induction of electric current

• Self-excited dynamo: inducing magnetic field created by the electric current (Siemens 1867)

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## Homopolar dynamo



electromotive force  $u \times B \sim$  electric current through wire loop  $\sim$  induced magnetic field reinforces applied magnetic field

self-excitation if rotation  $\Omega > 2\pi R/M$  is maintained where *R* resistance, *M* inductance

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# Geodynamo hypothesis

- Larmor (1919): Magnetic field of Earth and Sun maintained by self-excited dynamo
- Homogeneous dynamo (no wires in Earth core)
   ∼ complex motion necessary
- Kinematic (*u* prescribed, linear)
- Dynamic (*u* determined by forces, including Lorentz force, non-linear)

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Pre-Maxwell theory Induction equation Alfven theorem Magnetic Reynolds number and flux expulsion Poloidal and toroidal magnetic fields

## **Pre-Maxwell theory**

Maxwell equations:cgs system, vacuum, B = H, D = E $c \nabla \times B = 4\pi j + \frac{\partial E}{\partial t}$ , $c \nabla \times E = -\frac{\partial B}{\partial t}$ , $\nabla \cdot B = 0$ , $\nabla \cdot E = 4\pi \lambda$ 

#### Basic assumptions of MHD:

- $u \ll c$ : system stationary on light travel time, no em waves
- high electrical conductivity: *E* determined by  $\partial \mathbf{B}/\partial t$ , not by charges  $\lambda$

$$c\frac{E}{L} \approx \frac{B}{T} \sim \frac{E}{B} \approx \frac{1}{c}\frac{L}{T} \approx \frac{u}{c} \ll 1 , E \text{ plays minor role} : \frac{e_{el}}{e_m} \approx \frac{E^2}{B^2} \ll 1$$
$$\frac{\partial E/\partial t}{c\nabla \times B} \approx \frac{E/T}{cB/L} \approx \frac{E}{B}\frac{u}{c} \approx \frac{u^2}{c^2} \ll 1 , \text{ displacement current negligible}$$

**Pre-Maxwell equations:** 

$$c \nabla \times \boldsymbol{B} = 4\pi \boldsymbol{j}, \quad c \nabla \times \boldsymbol{E} = -\frac{\partial \boldsymbol{B}}{\partial t}, \quad \nabla \cdot \boldsymbol{B} = 0$$

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## Pre-Maxwell theory

Pre-Maxwell equations Galilei-covariant:

$$\mathbf{E}' = \mathbf{E} + \frac{1}{c}\mathbf{u} \times \mathbf{B}, \quad \mathbf{B}' = \mathbf{B}, \quad \mathbf{j}' = \mathbf{j}$$

Relation between **j** and **E** by Galilei-covariant **Ohm's law:**  $\mathbf{j}' = \sigma \mathbf{E}'$ in resting frame of reference,  $\sigma$  electrical conductivity

$$\boldsymbol{j} = \sigma(\boldsymbol{E} + \frac{1}{c}\boldsymbol{u} \times \boldsymbol{B})$$

Magnetohydrokinematics:

$$c\nabla \times B = 4\pi j$$
  

$$c\nabla \times E = -\frac{\partial B}{\partial t}$$
  

$$\nabla \cdot B = 0$$
  

$$j = \sigma(E + \frac{1}{c}u \times B)$$

Magnetohydrodynamics:

additionally

Equation of motion Equation of continuity Equation of state Energy equation

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## Induction equation

#### Evolution of magnetic field

$$\frac{\partial \boldsymbol{B}}{\partial t} = -c\boldsymbol{\nabla}\times\boldsymbol{E} = -c\boldsymbol{\nabla}\times\left(\frac{\boldsymbol{j}}{\sigma} - \frac{1}{c}\boldsymbol{u}\times\boldsymbol{B}\right) = -c\boldsymbol{\nabla}\times\left(\frac{c}{4\pi\sigma}\boldsymbol{\nabla}\times\boldsymbol{B} - \frac{1}{c}\boldsymbol{u}\times\boldsymbol{B}\right)$$
$$= \boldsymbol{\nabla}\times(\boldsymbol{u}\times\boldsymbol{B}) - \boldsymbol{\nabla}\times\left(\frac{c^2}{4\pi\sigma}\boldsymbol{\nabla}\times\boldsymbol{B}\right) = \boldsymbol{\nabla}\times(\boldsymbol{u}\times\boldsymbol{B}) - \eta\boldsymbol{\nabla}\times\boldsymbol{\nabla}\times\boldsymbol{B}$$
with  $\eta = \frac{c^2}{4\pi\sigma} = \text{const}$  magnetic diffusivity

induction, diffusion

 $abla imes (\mathbf{u} imes \mathbf{B}) = -\mathbf{B} \, 
abla \cdot \mathbf{u} + (\mathbf{B} \cdot 
abla) \mathbf{u} - (\mathbf{u} \cdot 
abla) \mathbf{B}$ 

expansion/contraction, shear/stretching, advection

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## Alfven theorem

Ideal conductor 
$$\eta = 0$$
 :  $\frac{\partial \boldsymbol{B}}{\partial t} = \boldsymbol{\nabla} \times (\boldsymbol{u} \times \boldsymbol{B})$ 

Magnetic flux through floating surface is constant :

$$\frac{d}{dt}\int_{F}\boldsymbol{B}\cdot d\boldsymbol{F}=0$$

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Proof:

$$0 = \int \nabla \cdot \mathbf{B} d\mathbf{V} = \int \mathbf{B} \cdot d\mathbf{F} = \int_{F} \mathbf{B}(t) \cdot d\mathbf{F} - \int_{F'} \mathbf{B}(t) \cdot d\mathbf{F}' - \oint_{C} \mathbf{B}(t) \cdot d\mathbf{s} \times u dt$$
$$\int_{F'} \mathbf{B}(t+dt) \cdot d\mathbf{F}' - \int_{F} \mathbf{B}(t) \cdot d\mathbf{F} = \int_{F} \{\mathbf{B}(t+dt) - \mathbf{B}(t)\} \cdot d\mathbf{F} - \oint_{C} \mathbf{B} \cdot d\mathbf{s} \times u dt$$
$$= dt \left(\int \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{F} - \oint_{C} \mathbf{B} \cdot d\mathbf{s} \times u\right) = dt \left(\int \nabla \times (\mathbf{u} \times \mathbf{B}) \cdot d\mathbf{F} - \oint_{C} \mathbf{B} \cdot d\mathbf{s} \times u\right)$$
$$= dt \left(\oint_{C} \mathbf{u} \times \mathbf{B} \cdot d\mathbf{s} - \oint_{C} \mathbf{B} \cdot d\mathbf{s} \times u\right) = 0$$



Basic electrodynamics Magnetohydrodynamical dynamos Alfven theorem

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## Alfven theorem



Frozen-in field lines

impression that magnetic field follows flow, but  $\mathbf{E} = -\mathbf{u} \times \mathbf{B}$  and  $\nabla \times \mathbf{E} = -c\partial \mathbf{B}/\partial t$ 

$$\frac{\partial \boldsymbol{B}}{\partial t} = \boldsymbol{\nabla} \times (\boldsymbol{u} \times \boldsymbol{B}) = -\boldsymbol{B} \, \boldsymbol{\nabla} \cdot \boldsymbol{u} + (\boldsymbol{B} \cdot \boldsymbol{\nabla}) \boldsymbol{u} - (\boldsymbol{u} \cdot \boldsymbol{\nabla}) \boldsymbol{B}$$

(i) star contraction:  $\overline{B} \sim R^{-2}$ ,  $\overline{\rho} \sim R^{-3} \sim \overline{B} \sim \overline{\rho}^{2/3}$ Sun  $\sim$  white dwarf  $\sim$  neutron star:  $\rho$  [g cm<sup>-3</sup>]: 1  $\sim$  10<sup>6</sup>  $\sim$  10<sup>15</sup> (ii) stretching of flux tube:  $() \rightarrow \bullet$  $Bd^2 = \text{const.} \ ld^2 = \text{const.} \sim B \sim l$ (iii) shear, differential rotation

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## **Differential rotation**

 $\partial B_{\phi}/\partial t = r \sin \theta \, \nabla \Omega \cdot \boldsymbol{B}_{\rho}$ 





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## Magnetic Reynolds number

Dimensionless variables: length L, velocity  $u_0$ , time  $L/u_0$ 

$$\frac{\partial \boldsymbol{B}}{\partial t} = \boldsymbol{\nabla} \times (\boldsymbol{u} \times \boldsymbol{B}) - \boldsymbol{R}_m^{-1} \, \boldsymbol{\nabla} \times \boldsymbol{\nabla} \times \boldsymbol{B} \quad \text{with} \quad \boldsymbol{R}_m = \frac{u_0 L}{\eta}$$

as combined parameter

```
laboratorium: R_m \ll 1, cosmos: R_m \gg 1
induction for R_m \gg 1, diffusion for R_m \ll 1, e.g. for small L
example: flux expulsion from closed velocity fields
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## Flux expulsion



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Geomagnetic Dynamo Theory

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## Poloidal and toroidal magnetic fields

Spherical coordinates  $(r, \vartheta, \varphi)$ 

Axisymmetric fields:  $\partial/\partial \varphi = 0$ 

$$\begin{split} \boldsymbol{B}(r,\vartheta) &= (B_r, B_\vartheta, B_\varphi) \\ \boldsymbol{\nabla} \cdot \boldsymbol{B} &= 0 \\ \boldsymbol{B} &= \boldsymbol{B}_p + \boldsymbol{B}_t \text{ poloidal and toroidal magnetic field} \\ \boldsymbol{B}_t &= (0, 0, B_\varphi) \text{ satisfies } \boldsymbol{\nabla} \cdot \boldsymbol{B}_t = 0 \\ \boldsymbol{B}_p &= (B_r, B_\vartheta, 0) = \boldsymbol{\nabla} \times \boldsymbol{A} \text{ with } \boldsymbol{A} = (0, 0, A_\varphi) \text{ satisfies } \boldsymbol{\nabla} \cdot \boldsymbol{B}_p = 0 \\ \boldsymbol{B}_p &= \frac{1}{r \sin \vartheta} \left( \frac{\partial r \sin \vartheta A_\varphi}{r \partial \vartheta}, -\frac{\partial r \sin \vartheta A_\varphi}{\partial r}, 0 \right) \end{split}$$

axisymmetric magnetic field determined by the two scalars:  $r \sin \vartheta A_{\varphi}$  and  $B_{\varphi}$ 

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## Poloidal and toroidal magnetic fields

Axisymmetric fields:

$$m{j}_t = rac{c}{4\pi} m{
abla} imes m{B}_
ho \;, \quad m{j}_
ho = rac{c}{4\pi} m{
abla} imes m{B}_t$$

 $r \sin \vartheta A_{\varphi} = \text{const}$ : field lines of poloidal field in meridional plane field lines of  $\boldsymbol{B}_t$  are circles around symmetry axis

Non-axisymmetric fields:

$$B = B_p + B_t = \nabla \times \nabla \times (Pr) + \nabla \times (Tr) = -\nabla \times (r \times \nabla P) - r \times \nabla T$$
  

$$r = (r, 0, 0), \quad P(r, \vartheta, \varphi) \quad \text{and} \quad T(r, \vartheta, \varphi) \quad \text{defining scalars}$$
  

$$\nabla \cdot B = 0, \quad \mathbf{j}_t = \frac{c}{4\pi} \nabla \times \mathbf{B}_p, \quad \mathbf{j}_p = \frac{c}{4\pi} \nabla \times \mathbf{B}_t$$
  

$$r \cdot \mathbf{B} = 0, \quad \text{field lines of the toroidal field lie on spheres, no recommendations}$$

 $\mathbf{r} \cdot \mathbf{B}_t = 0$  field lines of the toroidal field lie on spheres, no r component

 $\boldsymbol{B}_{p}$  has in general all three components

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# Cowling's theorem (Cowling 1934)

Axisymmetric magnetic fields can not be maintained by a dynamo.

Sketch of proof:

- electric currents as sources of the magnetic field only in finite space
- field line *F* = 0 along axis closes at infinity
- field lines on circular tori whose cross section are the lines F = const



- axisymmetry: closed neutral line
- around neutral line is  $\nabla \times \boldsymbol{B} \neq 0 \quad \sim \quad j_{\varphi} \neq 0$ , but there is no source of  $j_{\varphi}$ :  $E_{\varphi} = 0$  because of axisymmetry and  $(\boldsymbol{u} \times \boldsymbol{B})_{\varphi} = 0$  on neutral line for finite  $\boldsymbol{u}$ .

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# Cowling's theorem

Consider vicinity of neutral line, assume axisymmetry

$$\oint B_{p} dI = \oint \mathbf{B} \cdot d\mathbf{I} = \int \nabla \times \mathbf{B} \, d\mathbf{f} = \frac{4\pi}{c} \int \mathbf{j} \cdot d\mathbf{f} = \frac{4\pi}{c} \int |j_{\varphi}| df$$
$$= \frac{4\pi\sigma}{c^{2}} \int |\mathbf{u}_{p} \times \mathbf{B}_{p}| df \le \frac{4\pi\sigma}{c^{2}} \int u_{p} B_{p} df \le \frac{4\pi\sigma}{c^{2}} u_{p,\max} \int B_{p} df$$

integration circle of radius  $\varepsilon$ 

$$\begin{split} B_{p} 2\pi\varepsilon &\leq \frac{4\pi\sigma}{c^{2}} u_{\text{p,max}} B_{p} \pi\varepsilon^{2} \quad \text{or} \quad 1 \leq \frac{2\pi\sigma}{c^{2}} u_{\text{p,max}} \varepsilon \\ \varepsilon &\to 0 \quad \curvearrowright \quad u_{\text{p,max}} \to \infty \\ \text{contradiction} \end{split}$$

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## Toroidal theorems

Toroidal velocity theorem (Elsasser 1947, Bullard & Gellman 1954)

A toroidal motion in a spherical conductor can not maintain a magnetic field by dynamo action.

Sketch of proof:

$$\frac{d}{dt}(\mathbf{r} \cdot \mathbf{B}) = \eta \nabla^2(\mathbf{r} \cdot \mathbf{B}) \quad \text{for} \quad \mathbf{r} \cdot \mathbf{u} = 0$$
  
$$\sim \mathbf{r} \cdot \mathbf{B} \to 0 \quad \text{for} \quad t \to \infty \quad \curvearrowright \quad P \to 0 \quad \curvearrowright \quad T \to 0$$

#### Toroidal field theorem / Invisible dynamo theorem (Kaiser et al. 1994)

A purely toroidal magnetic field can not be maintained by a dynamo.

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## Parker's helical convection



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## Mean-field theory

Statistical consideration of turbulent helical convection on mean magnetic field (Steenbeck, Krause and Rädler 1966)

 $\frac{\partial \boldsymbol{B}}{\partial t} = \boldsymbol{\nabla} \times (\boldsymbol{u} \times \boldsymbol{B}) - \eta \boldsymbol{\nabla} \times \boldsymbol{\nabla} \times \boldsymbol{B}$  $u = \overline{u} + u'$ ,  $B = \overline{B} + B'$  Reynolds rules for averages  $\frac{\partial \overline{\boldsymbol{B}}}{\partial t} = \boldsymbol{\nabla} \times (\overline{\boldsymbol{u}} \times \overline{\boldsymbol{B}} + \boldsymbol{\mathcal{E}}) - \eta \boldsymbol{\nabla} \times \boldsymbol{\nabla} \times \boldsymbol{B}$  $\mathcal{E} = \mathbf{u'} \times \mathbf{B'}$  mean electromotive force  $\frac{\partial \mathbf{B}'}{\partial t} = \mathbf{\nabla} \times (\overline{\mathbf{u}} \times \mathbf{B}' + \mathbf{u}' \times \overline{\mathbf{B}} + \mathbf{G}) - \eta \mathbf{\nabla} \times \mathbf{\nabla} \times \mathbf{B}'$  $G = u' \times B' - \overline{u' \times B'}$  usually neglected, FOSA = SOCA B' linear, homogeneous functional of B approximation of scale separation: B' depends on  $\overline{B}$  only in small surrounding Taylor expansion:  $(\overline{u' \times B'})_i = \alpha_{ij}\overline{B}_i + \beta_{ijk}\partial\overline{B}_k/\partial x_i + \dots$ 

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## Mean-field theory

$$\begin{split} & \left(\overline{\boldsymbol{u}' \times \boldsymbol{B}'}\right)_i = \alpha_{ij}\overline{B}_j + \beta_{ijk}\partial\overline{B}_k/\partial x_j + \dots \\ & \alpha_{ij} \text{ and } \beta_{ijk} \text{ depend on } \boldsymbol{u}' \\ & \text{homogeneous, isotropic } \boldsymbol{u}' : \alpha_{ij} = \alpha\delta_{ij} , \ \beta_{ijk} = -\beta\varepsilon_{ijk} \text{ then} \\ & \overline{\boldsymbol{u}' \times \boldsymbol{B}'} = \alpha \overline{\boldsymbol{B}} - \beta \nabla \times \overline{\boldsymbol{B}} \\ & \text{Ohm's law: } \boldsymbol{j} = \sigma(\boldsymbol{E} + (\boldsymbol{u} \times \boldsymbol{B})/c) \\ & \boldsymbol{\bar{j}} = \sigma(\overline{\boldsymbol{E}} + (\overline{\boldsymbol{u}} \times \overline{\boldsymbol{B}})/c + (\alpha \overline{\boldsymbol{B}} - \beta \nabla \times \overline{\boldsymbol{B}})/c) \text{ and } c \nabla \times \overline{\boldsymbol{B}} = 4\pi \boldsymbol{\bar{j}} \\ & \boldsymbol{\bar{j}} = \sigma_{\text{eff}}(\overline{\boldsymbol{E}} + (\overline{\boldsymbol{u}} \times \overline{\boldsymbol{B}})/c + \alpha \overline{\boldsymbol{B}}/c) \\ & \frac{\partial \overline{\boldsymbol{B}}}{\partial t} = \nabla \times (\overline{\boldsymbol{u}} \times \overline{\boldsymbol{B}} + \alpha \overline{\boldsymbol{B}}) - \eta_{\text{eff}} \nabla \times \nabla \times \overline{\boldsymbol{B}} \text{ with } \eta_{\text{eff}} = \eta + \beta \\ & \text{Two effects:} \\ & (1) \ \alpha - \text{effect: } \quad \boldsymbol{\bar{j}} = \sigma_{\text{eff}} \alpha \overline{\boldsymbol{B}}/c \\ & (2) \text{ turbulent diffusivity: } \beta \gg \eta , \quad \eta_{\text{eff}} = \beta = \eta_T \end{split}$$

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## Sketch of dependence of $\alpha$ and $\beta$ on u'

$$\frac{\partial \mathbf{B}'}{\partial t} = \mathbf{\nabla} \times (\mathbf{\overline{u}} \times \mathbf{B}' + \mathbf{u}' \times \mathbf{\overline{B}} + \mathbf{G}) - \eta \mathbf{\nabla} \times \mathbf{\nabla} \times \mathbf{B}'$$

simplifying assumptions:  ${\cal G}=0$  ,  ${\it u}'$  incompressible, isotropic ,  $\overline{{\it u}}=0$  ,  $\eta=0$ 

$$\begin{split} \mathbf{B}_{k}^{\prime} &= \int_{t_{0}}^{t} \underbrace{\mathfrak{E}_{klm} \mathfrak{E}_{mrs}}_{\delta_{kr} \delta_{ls} - \delta_{ks} \delta_{lr}} \frac{\partial}{\partial x_{l}} (u_{r}^{\prime} \overline{B}_{s}) d\tau + B_{k}^{\prime}(t_{0}) \\ \mathbf{E}_{i} &= \langle \mathbf{u}^{\prime} \times \mathbf{B}^{\prime} \rangle_{i} = \mathfrak{E}_{ijk} \Big\langle u_{j}^{\prime}(t) \Big[ \int_{t_{0}}^{t} \Big( \frac{\partial u_{k}^{\prime}}{\partial x_{l}} \overline{B}_{l} + u_{k}^{\prime} \frac{\partial \overline{B}_{l}}{\partial x_{l}} - \frac{\partial u_{l}^{\prime}}{\partial x_{l}} \overline{B}_{k} - u_{l}^{\prime} \frac{\partial \overline{B}_{k}}{\partial x_{l}} \Big) d\tau + B_{k}^{\prime}(t_{0}) \Big] \Big\rangle \\ &= \mathfrak{E}_{ijk} \int_{t_{0}}^{t} \Big[ \underbrace{ \Big\langle u_{j}^{\prime}(t) \frac{\partial u_{k}^{\prime}(\tau)}{\partial x_{l}} \Big\rangle}_{\sim \alpha} \overline{B}_{l} - \underbrace{ \Big\langle u_{j}^{\prime}(t) u_{l}^{\prime}(\tau) \Big\rangle}_{\sim \beta} \frac{\partial \overline{B}_{k}}{\partial x_{l}} \Big] d\tau \\ &\text{isotropic turbulence: } \alpha = -\frac{1}{3} \overline{\mathbf{u}^{\prime} \cdot \nabla \times \mathbf{u}^{\prime}} \tau^{*} = -\frac{1}{3} \overline{H} \tau^{*} \quad \text{and} \quad \beta = \frac{1}{3} u^{\prime 2} \tau^{*} \\ H \text{ belicity} \quad \tau^{*} \text{ correlation time} \end{split}$$

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### Mean-field coefficients derived from a MHD geodynamo simulation



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## Mean-field dynamos

Dynamo equation:

$$\frac{\partial \mathbf{B}}{\partial t} = \mathbf{\nabla} \times (\overline{\mathbf{u}} \times \overline{\mathbf{B}} + \alpha \overline{\mathbf{B}} - \eta_T \mathbf{\nabla} \times \overline{\mathbf{B}})$$

- spherical coordinates, axisymmetry
- $\overline{\boldsymbol{u}} = (0, 0, \Omega(r, \vartheta) r \sin \vartheta)$

• 
$$\overline{\boldsymbol{B}} = (0, 0, B(r, \vartheta, t)) + \nabla \times (0, 0, A(r, \vartheta, t))$$

$$\frac{\partial B}{\partial t} = r \sin \vartheta (\nabla \times \mathbf{A}) \cdot \nabla \Omega - \alpha \nabla_1^2 \mathbf{A} + \eta_T \nabla_1^2 \mathbf{B}$$
$$\frac{\partial A}{\partial t} = \alpha \mathbf{B} + \eta_T \nabla_1^2 \mathbf{A} \quad \text{with} \quad \nabla_1^2 = \nabla^2 - (r \sin \vartheta)^{-2}$$



rigid rotation has no effect

no dynamo if  $\alpha = 0$ 

$$\frac{\alpha - \text{term}}{\nabla \Omega - \text{term}} \approx \frac{\alpha_0}{|\nabla \Omega| L^2} \quad \begin{cases} \gg 1 & \alpha^2 - \text{dynamo with dynamo number } R_{\alpha}^2 \\ \ll 1 & \alpha \Omega - \text{dynamo with dynamo number } R_{\alpha} R_{\Omega} \end{cases}$$

Antidynamo theorems Parker's helical convection Mean-field theory Mean-field coefficients Mean-field dynamos

## Sketch of an $\alpha\Omega$ dynamo



periodically alternating field, here antisymmetric with respect to equator

Antidynamo theorems Parker's helical convection Mean-field theory Mean-field coefficients Mean-field dynamos

## Sketch of an $\alpha^2$ dynamo



stationary field, here antisymmetric with respect to equator

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MHD equations of rotating fluids in non-dimensional form

Navier-Stokes equation including Coriolis and Lorentz forces

$$E\left(\frac{\partial \boldsymbol{u}}{\partial t} + \boldsymbol{u} \cdot \boldsymbol{\nabla} \boldsymbol{u} - \boldsymbol{\nabla}^2 \boldsymbol{u}\right) + 2\hat{\boldsymbol{z}} \times \boldsymbol{u} + \boldsymbol{\nabla} \Pi = Ra\frac{\boldsymbol{r}}{r_0}T + \frac{1}{Pm}(\boldsymbol{\nabla} \times \boldsymbol{B}) \times \boldsymbol{B}$$
  
Inertia Viscosity Coriolis Buoyancy Lorentz

#### Induction equation

$$\frac{\partial \boldsymbol{B}}{\partial t} = \boldsymbol{\nabla} \times (\boldsymbol{u} \times \boldsymbol{B}) - \frac{1}{Pm} \boldsymbol{\nabla} \times \boldsymbol{\nabla} \times \boldsymbol{B}$$
  
Induction Diffusion

#### **Energy equation**

$$\frac{\partial T}{\partial t} + \boldsymbol{u} \cdot \boldsymbol{\nabla} T = \frac{1}{Pr} \boldsymbol{\nabla}^2 T + Q$$

Incompressibility and divergence-free magnetic field

$$\boldsymbol{
abla}\cdot\boldsymbol{u}=0$$
 ,  $\boldsymbol{
abla}\cdot\boldsymbol{B}=0$ 

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## Non-dimensional parameters

#### **Control parameters (Input)**

Parameter	Definition	Force balance	Model value	Earth value
Rayleigh number	$Ra = \alpha g_0 \Delta T d / v \Omega$	buoyancy/diffusivity	1 – 50 <i>Ra</i> <sub>crit</sub>	≫ <i>Ra</i> <sub>crit</sub>
Ekman number	$E = v/\Omega d^2$	viscosity/Coriolis	$10^{-6} - 10^{-4}$	10 <sup>-14</sup>
Prandtl number	$Pr = v/\kappa$	viscosity/thermal diff.	$2 \cdot 10^{-2} - 10^3$	0.1 – 1
Magnetic Prandtl	$Pm = \nu/\eta$	viscosity/magn. diff.	$10^{-1} - 10^3$	$10^{-6} - 10^{-5}$

#### **Diagnostic parameters (Output)**

Definition	Force balance	Model value	Earth value
$\Lambda = B^2/\mu ho\eta\Omega$	Lorentz/Coriolis	0.1 – 100	0.1 – 10
Re = ud/v	inertia/viscosity	< 500	10 <sup>8</sup> – 10 <sup>9</sup>
$Rm = ud/\eta$	induction/magn. diff.	50 – 10 <sup>3</sup>	10 <sup>2</sup> – 10 <sup>3</sup>
$Ro = u/\Omega d$	inertia/Coriolis	$3 \cdot 10^{-4} - 10^{-2}$	$10^{-7} - 10^{-6}$
	$\begin{aligned} & \textbf{Definition} \\ & \Lambda = B^2/\mu\rho\eta\Omega \\ & Re = ud/\nu \\ & Rm = ud/\eta \\ & Ro = u/\Omegad \end{aligned}$	DefinitionForce balance $\Lambda = B^2/\mu\rho\eta\Omega$ Lorentz/Coriolis $Re = ud/\nu$ inertia/viscosity $Rm = ud/\eta$ induction/magn. diff. $Ro = u/\Omega d$ inertia/Coriolis	$\begin{array}{lll} \mbox{Definition} & \mbox{Force balance} & \mbox{Model value} \\ \Lambda = B^2/\mu\rho\eta\Omega & \mbox{Lorentz/Coriolis} & 0.1-100 \\ Re = ud/\nu & \mbox{inertia/viscosity} & < 500 \\ Rm = ud/\eta & \mbox{induction/magn. diff.} & 50-10^3 \\ Ro = u/\Omegad & \mbox{inertia/Coriolis} & 3\cdot10^{-4}-10^{-2} \end{array}$

Earth core values:  $d \approx 2 \cdot 10^5$  m,  $u \approx 2 \cdot 10^{-4}$  m s<sup>-1</sup>,  $v \approx 10^{-6}$  m<sup>2</sup>s<sup>-1</sup>

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## Proudman-Taylor theorem

Non-magnetic hydrodynamics in rapidly rotating system

 $E \ll 1$ ,  $Ro \ll 1$ : viscosity and inertia small

balance between Coriolis force and pressure gradient

$$-oldsymbol{
abla}
ho=2
hooldsymbol{\Omega} imesoldsymbol{u}$$
 ,  $oldsymbol{
abla} imes\colon (oldsymbol{\Omega}m{\cdot}oldsymbol{
abla})oldsymbol{u}=0$ 

 $\frac{\partial \mathbf{u}}{\partial z} = 0$  motion independent along axis of rotation, geostrophic motion

(Proudman 1916, Taylor 1921)

#### **Ekman layer:**

At fixed boundary  $\boldsymbol{u} = 0$ , violation of P.-T. theorem necessary for motion close to boundary allow viscous stresses  $v \nabla^2 \boldsymbol{u}$  for gradients of  $\boldsymbol{u}$  in *z*-direction Ekman layer of thickness  $\delta_l \sim E^{1/2}L \sim 0.2$  m for Earth core

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## Convection in rotating spherical shell



inside tangent cylinder: *g* || Ω: Coriolis force opposes convection outside tangent cylinder:

P.-T. theorem leads to columnar convection cells  $exp(im\varphi - \omega t)$  dependence at onset of convection, 2m columns which drift in  $\varphi$ -direction

• • • • • • • •

inclined outer boundary violates Proudman-Taylor theorem

 $\sim$  columns close to tangent cylinder around inner core inclined boundaries, Ekman pumping and inhomogeneous thermal buoyancy lead to secondary circulation along convection columns: poleward in columns with  $\omega_z < 0$ , equatorward in columns with  $\omega_z > 0$  $\sim$  negative helicity north of the equator and positive one south

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## Convection in rotating spherical shell





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## Taylor's constraint

$$2\rho \Omega \times \boldsymbol{u} = -\nabla p + \rho \boldsymbol{g} + (\nabla \times \boldsymbol{B}) \times \boldsymbol{B}/4\pi$$
 magnetostrophic regime  
 $\nabla \cdot \boldsymbol{u} = 0$ ,  $\rho = \text{const}$ ;  $\Omega = \omega_0 \boldsymbol{e}_z$ 

Consider  $\varphi$ -component and integrate over cylindrical surface C(s)

 $\partial p / \partial \varphi = 0$  after integration over  $\varphi$ , **g** in meridional plane

$$2\rho\Omega \underbrace{\int_{C(s)} \boldsymbol{u} \cdot d\boldsymbol{s}}_{=\boldsymbol{0}} = \frac{1}{4\pi} \int_{C(s)} \left( (\boldsymbol{\nabla} \times \boldsymbol{B}) \times \boldsymbol{B} \right)_{\varphi} ds$$
$$\int_{C(s)} \left( (\boldsymbol{\nabla} \times \boldsymbol{B}) \times \boldsymbol{B} \right)_{\varphi} ds = 0 \quad \text{(Taylor 1963)}$$



net torque by Lorentz force on any cylinder  $\parallel \Omega$  vanishes

*B* not necessarily small, but positive and negative parts of the integrand cancelling each other out

violation by viscosity in Ekman boundary layers ~ torsional oscillations around Taylor state

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## Benchmark dynamo

### $Ra = 10^5 = 1.8 \, Ra_{crit} \, , \quad E = 10^{-3} \, , \quad Pr = 1 \, , \quad Pm = 5$



Basic electrodynamics Magnetohydrodynamical dynamos Geodynamo simulations Interpretation

## Conversion of toroidal field into poloidal field



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## Generation of toroidal field from poloidal field



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## Field line bundle in the benchmark dynamo



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## Strongly driven dynamo model

 $Ra = 1.2 \times 10^8 = 42 Ra_{crit}$ ,  $E = 3 \times 10^{-5}$ , Pr = 1, Pm = 2.5



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## Comparison of the radial magnetic field at the CMB



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## Dynamical Magnetic Field Line Imaging / Movie 2



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## Reversals



500 years before midpoint

midpoint

500 years after midpoint

(Glatzmaier and Roberts 1995)

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## Reversals



, (Aubert et al. 2008)

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## Power requirement of the geodynamo

- Dynamo converts thermal and gravitational energy into magnetic energy
- Power requirement for geodynamo set by its ohmic losses
- Difficult to estimate: 0.1 5 TW  $\sim$  0.3 10% Earth's surface heat flow
- Recent estimate from numerical and laboratory dynamos by extrapolating the magnetic dissipation time for realistic values of the control parameters: 0.2 - 0.5 TW (Christensen and Tilgner 2004)
- Important for thermal budget and evolution of the inner core
- Thermal convection thermodynamically inefficient, compositional convection associated with core cooling
- High heat flow leads to rapid growth of the inner core and low age  $\leq$  1 Gyr
- Low power requirement estimated by Christensen and Tilgner (2004) is consistent with an inner core as old as 3.5 Gyr

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